

Eq. de Cauchy

$$\rho \frac{D\vec{v}}{Dt} = \nabla \cdot \underline{\underline{\sigma}} + \int \underline{\underline{g}} \quad (1)$$

↳ tensor de tensões?

Como modelar $\underline{\underline{\sigma}}$?

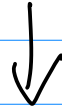
↳ eq. constitutiva

Versão diferencial do princípio de

Balanco de momento angular

$$\vec{T} \cdot \vec{T} \cdot \vec{R} \rightarrow \frac{D}{Dt} \int_V \underline{\underline{C}} dV = \int_V \left(\frac{D\underline{\underline{C}}}{Dt} + \underline{\underline{C}} \nabla \cdot \vec{v} \right) dV$$

$$\boxed{G = \underline{x} \times \underline{p} \underline{v}} \rightarrow T.T.R$$



$$\frac{D}{Dt} \int_V \underline{x} \times \underline{p} \underline{v} dV = \sum \underline{T} \quad (2)$$

lei física

Aplicando o T.T.R no primeiro termo do lado esquerdo:

$$\frac{D}{Dt} \int_V \underline{x} \times \underline{p} \underline{v} dV = \int_V \left[\frac{D}{Dt} (\underline{x} \times \underline{p} \underline{v}) + (\underline{x} \times \underline{p} \underline{v}) \nabla \cdot \underline{x} \right] dV$$

Note que: $G = pA$ ↳ muito complicado

$$T.T.R: \quad \frac{D}{Dt} \int_V pA dV = \int_V \left[\frac{D}{Dt} (pA) + pA \nabla \cdot \underline{x} \right] dV$$

$$\frac{D}{Dt} (\rho A) + \rho A \nabla \cdot \underline{v} = \rho \frac{DA}{Dt} + A \frac{D\rho}{Dt} + \rho A \nabla \cdot \underline{v}$$

$$= A \left(\frac{D\rho}{Dt} + \rho \nabla \cdot \underline{v} \right) + \rho \frac{DA}{Dt}$$

0, eq. da continuidade

Logo:

$$\frac{D}{Dt} \int_V \rho A dV = \int_V \rho \frac{DA}{Dt} dV$$

↳ consequência do T.T.R + eq. da continuidade

Até fim:

$$\int_V \rho \frac{D}{Dt} (\underline{x} \times \underline{v}) dV = \sum \underline{T} \quad (3)$$

↓
torques atuando
numa partícula flúida

$$\sum \underline{T} = \sum \underline{T}_s + \sum \underline{T}_V \rightarrow \text{volume} \quad (4)$$

↳ superfície

$$\sum \vec{T}_S = \int_S \vec{x} \times (\hat{n} \cdot \underline{\underline{\sigma}}) dS \quad (5)$$

$$\sum \vec{T}_V = \int_V \left(\vec{x} \times \rho \vec{g} + \vec{t}_V \right) dV \quad (6)$$

↓
densidade volumétrica de
torques internos (intrínsecos)
do material

Usando (3), (4), (5) e (6):

$$\int_V \rho \frac{D}{Dt} \left(\vec{x} \times \vec{v} \right) dV = \int_V \left(\rho \vec{x} \times \vec{g} + \vec{t}_V \right) dV + \int_S \vec{x} \times (\hat{n} \cdot \underline{\underline{\sigma}}) dS$$

$$\underbrace{\vec{x} \times \frac{D\vec{v}}{Dt} + \vec{v} \times \frac{D\vec{x}}{Dt}}_{\vec{v}} = \vec{x} \times \frac{D\vec{v}}{Dt}$$

$$\int_V \vec{x} \times \left(\rho \frac{D\vec{v}}{Dt} - \rho \vec{g} - \vec{t}_V \right) dV = \int_S \vec{x} \times (\hat{n} \cdot \underline{\underline{\sigma}}) dS \quad (7)$$

Note que: $\underline{\underline{x}} \times (\hat{n} \cdot \underline{\underline{\sigma}}) = x_a \hat{e}_a \times (\hat{m}_b \hat{e}_b \cdot \sigma_{cd} \hat{e}_c \hat{e}_d)$

$$= x_a \hat{e}_a \times (\hat{m}_b \sigma_{cd} \delta_{bc} \hat{e}_d) = x_a \hat{m}_b \sigma_{bd} \hat{e}_a \times \hat{e}_d$$

$$= x_a \hat{m}_b \sigma_{bd} \epsilon_{ade} \hat{e}_e = \epsilon_{ea} x_a \hat{m}_b \sigma_{bd}$$

$$\Rightarrow \epsilon_{ijk} x_j \hat{m}_p \sigma_{pk} = \underbrace{\epsilon_{ijk} x_j \sigma_{pk}}_{T_{ip}} \hat{m}_p$$

T.D. p/tensors de 2^a ordem:

$$\int_S T_{ip} \hat{m}_p dS = \int_S \hat{n} \cdot \underline{\underline{T}}^T dS = \int_V \nabla \cdot \underline{\underline{T}}^T dV$$

\downarrow T.D. \downarrow

Logo: $\int_S \underline{\underline{x}} \times (\hat{n} \cdot \underline{\underline{\sigma}}) dS = \int_V \frac{\partial}{\partial x_p} (\epsilon_{ijk} x_j \sigma_{pk}) dV$

$$= \int_V \epsilon_{ijk} \left(\underbrace{\frac{\partial x_j}{\partial x_p}}_{\delta_{jp}} \sigma_{pk} + x_j \frac{\partial \sigma_{pk}}{\partial x_p} \right) dV$$

$$= \int_V \left(\epsilon_{ijk} \sigma_{jk} + \epsilon_{ijk} x_j \frac{\partial \sigma_{pk}}{\partial x_p} \right) dV$$

$$\int_S \underline{\underline{x}} \times (\hat{n} \cdot \underline{\underline{\sigma}}) dS = \int_V \left[\underline{\underline{\varepsilon}} : \underline{\underline{\sigma}} + \underline{\underline{x}} \times (\nabla \cdot \underline{\underline{\sigma}}) \right] dV \quad (8)$$

(8) \rightarrow (7):

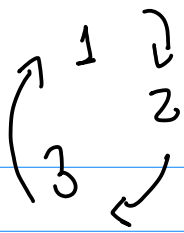
$$\int_V \underline{\underline{x}} \times \left[\rho \frac{D\underline{\underline{v}}}{Dt} - \rho \underline{\underline{g}} - \underline{\underline{t}}_v \right] dV = \int_V \left[\underline{\underline{\varepsilon}} : \underline{\underline{\sigma}} + \underline{\underline{x}} \times (\nabla \cdot \underline{\underline{\sigma}}) \right] dV$$

$$\int_V \left\{ \underline{\underline{x}} \times \left[\rho \frac{D\underline{\underline{v}}}{Dt} - \rho \underline{\underline{g}} - \nabla \cdot \underline{\underline{\sigma}} \right] - \underline{\underline{t}}_v - \underline{\underline{\varepsilon}} : \underline{\underline{\sigma}} \right\} dV = \underline{\underline{0}}$$

$\underline{\underline{0}} \rightarrow$ eq de Cauchy

$$\underline{\underline{\varepsilon}} : \underline{\underline{\sigma}} = -\underline{\underline{t}}_v \quad \rightarrow \text{ o que isto significa? }$$

$$\underline{\underline{\varepsilon}} : \underline{\underline{\sigma}} = \varepsilon_{ijk} \sigma_{jk}$$



$$\begin{aligned} \underline{\underline{\varepsilon}} : \underline{\underline{\sigma}} &= \left(\varepsilon_{1/23}^+ \sigma_{23} + \varepsilon_{1/32}^- \sigma_{32} \right) \hat{e}_1 \\ &+ \left(\varepsilon_{2/31}^+ \sigma_{31} + \varepsilon_{2/13}^- \sigma_{13} \right) \hat{e}_2 \\ &+ \left(\varepsilon_{3/12}^+ \sigma_{12} + \varepsilon_{3/21}^- \sigma_{21} \right) \hat{e}_3 \end{aligned}$$

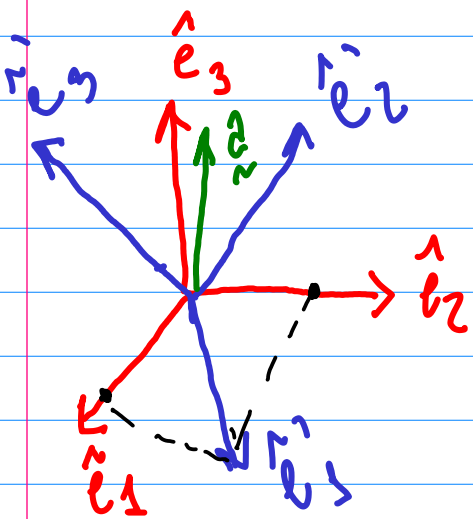
$$\begin{aligned} &= (\sigma_{23} - \sigma_{32}) \hat{e}_1 + (\sigma_{31} - \sigma_{13}) \hat{e}_2 \\ &\quad + (\sigma_{12} - \sigma_{21}) \hat{e}_3 = -\underline{\underline{t}}_v \end{aligned}$$

$$\text{Se } \underline{\underline{t}}_v = \underline{\underline{0}} \rightarrow \left. \begin{array}{l} \sigma_{23} = \sigma_{32} \\ \sigma_{31} = \sigma_{13} \\ \sigma_{12} = \sigma_{21} \end{array} \right\} \underline{\underline{\sigma}} = \underline{\underline{\sigma}}^T$$

"Na ausência de torques internos, intrinsicamente o material, o tensor de tensões do mesmo será sempre simétrico." \rightarrow Importante

Transformações ortogonais

Considere dois conjuntos de eixos ortogonais
com a mesma origem:



Sabemos que:

$$\hat{e}_i \cdot \hat{e}_j = \delta_{ij}$$

$$\hat{e}'_i \cdot \hat{e}'_j = \delta_{ij}$$

Seja representor $\underline{\tilde{a}}$ nos sistemas \hat{e}_i e \hat{e}'_i

$$\underline{\tilde{a}} = a_1 \hat{e}_1 + a_2 \hat{e}_2 + a_3 \hat{e}_3 = a_1 \hat{e}'_1 + a_2 \hat{e}'_2 + a_3 \hat{e}'_3$$

$\underline{\tilde{a}}$ é invariante. O que muda são suas componentes em cada escolha de S.C.

$$\begin{aligned} \underline{\hat{a}} &= \left[a_1' (\hat{e}_1' \cdot \hat{e}_1) + a_2' (\hat{e}_2' \cdot \hat{e}_1) + a_3' (\hat{e}_3' \cdot \hat{e}_1) \right] \hat{e}_1 \\ &+ \left[a_1' (\hat{e}_1' \cdot \hat{e}_2) + a_2' (\hat{e}_2' \cdot \hat{e}_2) + a_3' (\hat{e}_3' \cdot \hat{e}_2) \right] \hat{e}_2 \\ &+ \left[a_1' (\hat{e}_1' \cdot \hat{e}_3) + a_2' (\hat{e}_2' \cdot \hat{e}_3) + a_3' (\hat{e}_3' \cdot \hat{e}_3) \right] \hat{e}_3 \end{aligned}$$

$$a_i = a_j' \underbrace{(\hat{e}_j' \cdot \hat{e}_i)}_{\varphi_{ji}} \Rightarrow \left\{ \begin{array}{l} a_i = a_j' \varphi_{ji} \\ \underline{\hat{a}} = \underline{\varphi}^T \cdot \underline{\hat{a}}' \end{array} \right\}$$

Seja agora escrever \hat{e}_i em termos de \hat{e}_i' :

$$\hat{e}_1 = (\hat{e}_1' \cdot \hat{e}_1) \hat{e}_1' + (\hat{e}_1' \cdot \hat{e}_2) \hat{e}_2' + (\hat{e}_1' \cdot \hat{e}_3) \hat{e}_3'$$

$$\hat{e}_2 = (\hat{e}_2' \cdot \hat{e}_1) \hat{e}_1' + (\hat{e}_2' \cdot \hat{e}_2) \hat{e}_2' + (\hat{e}_2' \cdot \hat{e}_3) \hat{e}_3'$$

$$\hat{e}_3 = (\hat{e}_3' \cdot \hat{e}_1) \hat{e}_1' + (\hat{e}_3' \cdot \hat{e}_2) \hat{e}_2' + (\hat{e}_3' \cdot \hat{e}_3) \hat{e}_3'$$

$$\begin{aligned} \text{Como } \underline{\hat{a}} &= a_1 \hat{e}_1 + a_2 \hat{e}_2 + a_3 \hat{e}_3 = a_1' \hat{e}_1' + a_2' \hat{e}_2' + a_3' \hat{e}_3' \\ &= \underline{\hat{a}}' \end{aligned}$$

$$\begin{aligned} \hat{a}'_1 &= [\hat{a}_1 (\hat{e}_1 \cdot \hat{e}'_1) + \hat{a}_2 (\hat{e}_2 \cdot \hat{e}'_1) + \hat{a}_3 (\hat{e}_3 \cdot \hat{e}'_1)] \hat{e}'_1 \\ &+ [\hat{a}_1 (\hat{e}_1 \cdot \hat{e}'_2) + \hat{a}_2 (\hat{e}_2 \cdot \hat{e}'_2) + \hat{a}_3 (\hat{e}_3 \cdot \hat{e}'_2)] \hat{e}'_2 \\ &+ [\hat{a}_1 (\hat{e}_1 \cdot \hat{e}'_3) + \hat{a}_2 (\hat{e}_2 \cdot \hat{e}'_3) + \hat{a}_3 (\hat{e}_3 \cdot \hat{e}'_3)] \hat{e}'_3 \end{aligned}$$

$$a'_i = \hat{a}_j (\hat{e}_j \cdot \hat{e}'_i) = Q_{ij} \hat{a}_j$$

Até agora temos:

Lei de transformação de vetores

$$Q^T = Q^{-1}$$

$$\begin{aligned} \underline{\hat{a}} &= \underline{Q}^T \cdot \underline{\hat{a}'} \\ \underline{\hat{a}'} &= \underline{Q} \cdot \underline{\hat{a}} \end{aligned}$$

$$\begin{aligned} \underline{\hat{a}} &= \underline{Q}^T \cdot \underline{Q} \cdot \underline{\hat{a}} \\ &= \underline{I} \cdot \underline{\hat{a}} \end{aligned}$$

Relação de Ortogonalidade

Lei de Transformação p/ Tensores
Condições de 2^a ordem

Sejam \underline{a} e \underline{b} tensores simétricos de ordem 1,

logo: $a'_i = Q_{ip} a_p$ e $b'_j = Q_{jk} b_k$

$$e \quad a_i = \varphi_{pi} a_p' \quad e \quad b_j = \varphi_{kj} b_k'$$

Seja calcular $a_i b_j = T_{ij} = \varphi_{pi} \varphi_{kj} \underbrace{a_p' b_k'}_{T_{pk}}$

$$a_i' b_j' = T_{ij}' = \varphi_{ip} \varphi_{jk} \underbrace{a_p b_k}_{T_{pk}}$$

$$T_{ij}' = \varphi_{ip} \varphi_{jk} T_{pk}$$

ou

$$T_{ij} = \varphi_{pi} \varphi_{kj} T_{pk}'$$

$$\underline{\underline{T}} = \underline{\underline{\varphi}} \cdot \underline{\underline{T}} \cdot \underline{\underline{\varphi}}^T$$

ou

$$\underline{\underline{T}} = \underline{\underline{\varphi}}^T \cdot \underline{\underline{T}}' \cdot \underline{\underline{\varphi}}$$

↓
 Lei de transformação p/

tensores cartesianos de 2^{a} ordem

No caso mais geral p/ tensores de ordem "n":

$$T_{ijk\dots p} = Q_{li} Q_{mj} Q_{ok} Q_{rp} \dots T'_{lm\dots r}$$

Exemplo: tensor de 4^o ordem:

$$A_{ijkl} = Q_{ai} Q_{bj} Q_{ck} Q_{dl} A'_{abcd}$$

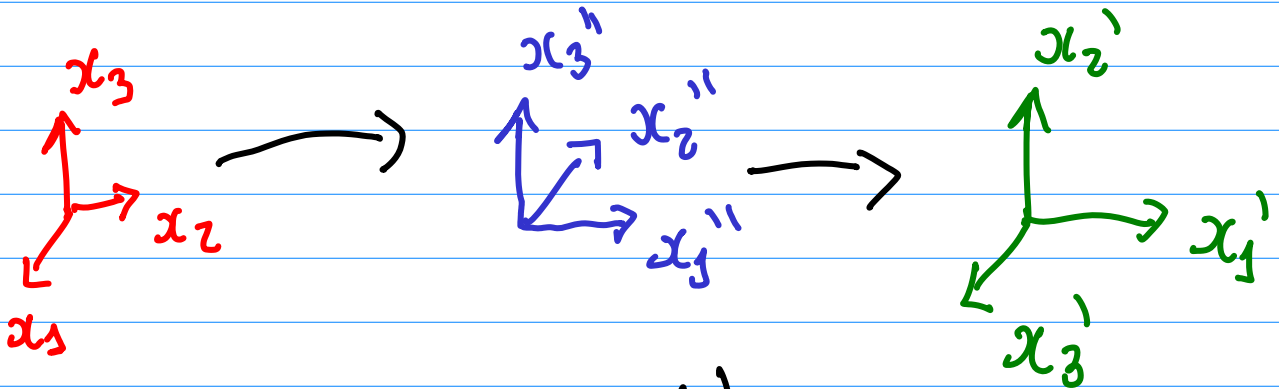
Tensores Isotrópicos

Def: Um tensor cujo os componentes permanecem invariantes a qualquer transformação ortogonal é dito isotrópico.

Teorema: Se T_{ij} são os componentes de um tensor isotrópico de 2^o ordem, então $T_{ij} = \alpha \delta_{ij}$, em que α é um campo escalar.

Demonstração

- Considere $T_{ij} = \alpha \delta_{ij}$ $\rightarrow T_{pp} = \alpha \delta_{pp}$
- Considere ainda a seguinte rotação de eixos:



$$\hat{e}_i \rightarrow \hat{e}'_i$$

$$\left. \begin{array}{l} \hat{e}'_1 = \hat{e}_2; \quad \hat{e}'_2 = \hat{e}_3; \quad \hat{e}'_3 = \hat{e}_1 \end{array} \right\}$$

$Q_{12} = Q_{23} = Q_{31} = 1$ e os outros termos são nulos!

$Q = \begin{pmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \end{pmatrix}$ Se T_{ij} é um tensor covariante de 2ª ordem, então o mesmo obedecerá à seguinte lei de transformação: $T'_{ij} = Q_{ip} Q_{jq} T_{pq}$

Adesso: $T'_{ij} = Q_{ip} Q_{jp} \kappa \delta_{pp} = \kappa Q_{ip} Q_{jp}$

Verificando componenti:

$$T'_{11} = \kappa Q_{1p} Q_{1p} = \kappa (Q_{11}^2 + Q_{12}^2 + Q_{13}^2) = \kappa$$

$$T'_{22} = \kappa Q_{2p} Q_{2p} = \kappa (Q_{21}^2 + Q_{22}^2 + Q_{23}^2) = \kappa$$

$$T'_{33} = \kappa Q_{3p} Q_{3p} = \kappa (Q_{31}^2 + Q_{32}^2 + Q_{33}^2) = \kappa$$

$$T'_{12} = \kappa Q_{1p} Q_{2p} = \kappa (\cancel{Q_{11} Q_{21}} + \cancel{Q_{12} Q_{22}} + \cancel{Q_{13} Q_{23}})$$

0 0 0

$$T'_{13} = T'_{21} = T'_{23} = T'_{31} = T'_{32} = T'_{12} = 0$$

$$\boxed{\underline{T'} = \kappa \underline{I} = \underline{T}}$$

Teorema de Cauchy-Weil

A forma mais geral de representação de um tensor isotrópico de 4^o ordem é:

$$T_{ijkl} = \alpha \delta_{ij} \delta_{kl} + \beta \delta_{ik} \delta_{jl} + \gamma \delta_{il} \delta_{jk}$$

↓
isotrópico